

**AM IBOC
Ascertainment Project
Corporation for Public
Broadcasting**

The dTR/H&D Joint Venture

A Joint Venture of duTreil, Lundin & Rackley and Hatfield & Dawson

Project Objectives

- Determine if AM IBOC can be successfully added to AM Public Radio Stations
- Provide Information that will optimize the performance of the AM Station for improvements to both Analogue and IBOC
- Identify Problem Installations
- Provide Suggestive Remedies for Conversion to IBOC

Project Components

- Site Visits to 53 CPB Qualified AM Stations from the Bering Sea to Puerto Rico
- Station Physical Inspection
- Antenna System Measurements
 - System Bandwidth
 - Directional System Performance

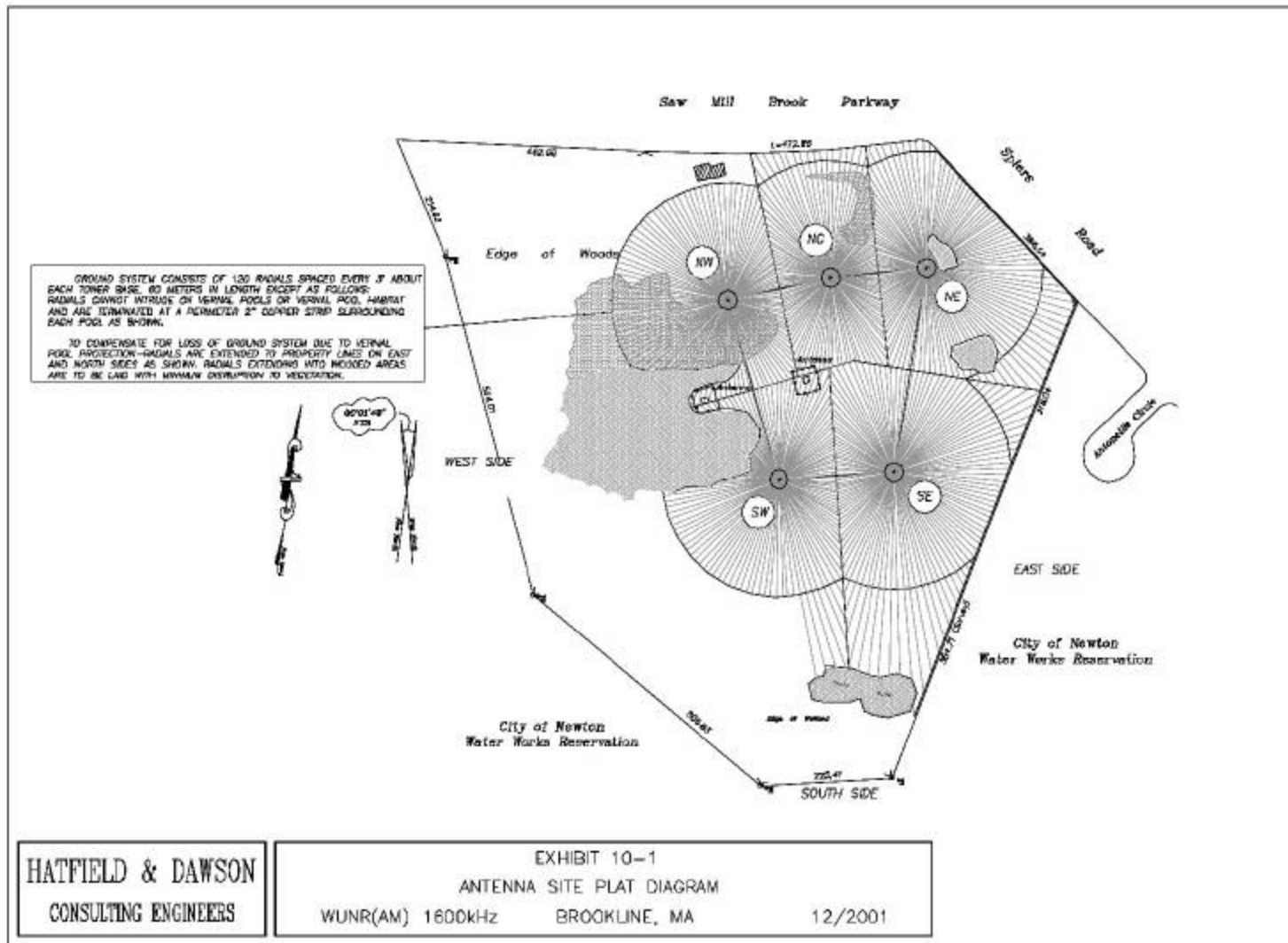


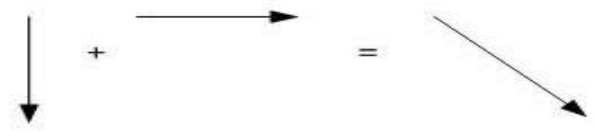
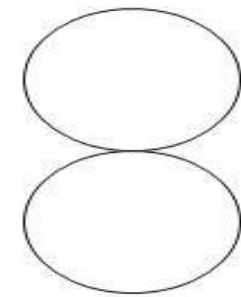
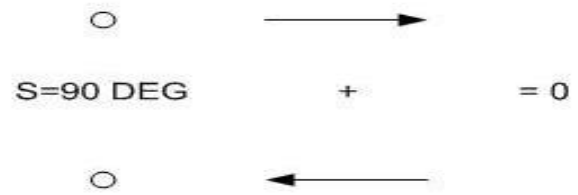
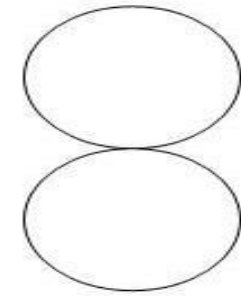
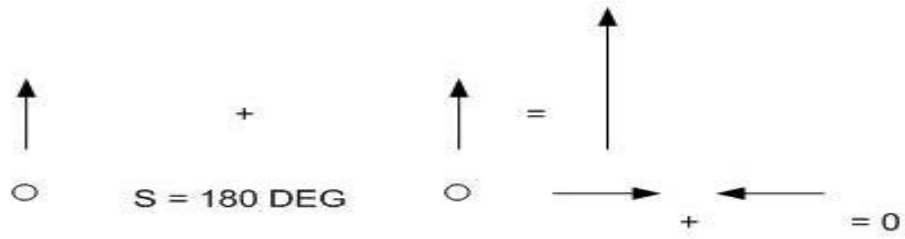


Project Analysis and Report

- Antenna System's compliance with Ibiquity's recommended "desired characteristics"
- Information for optimization for both IBOC and Analog system
- Report problems installations
- Recommendations for IBOC implementation

Directional Antenna Review



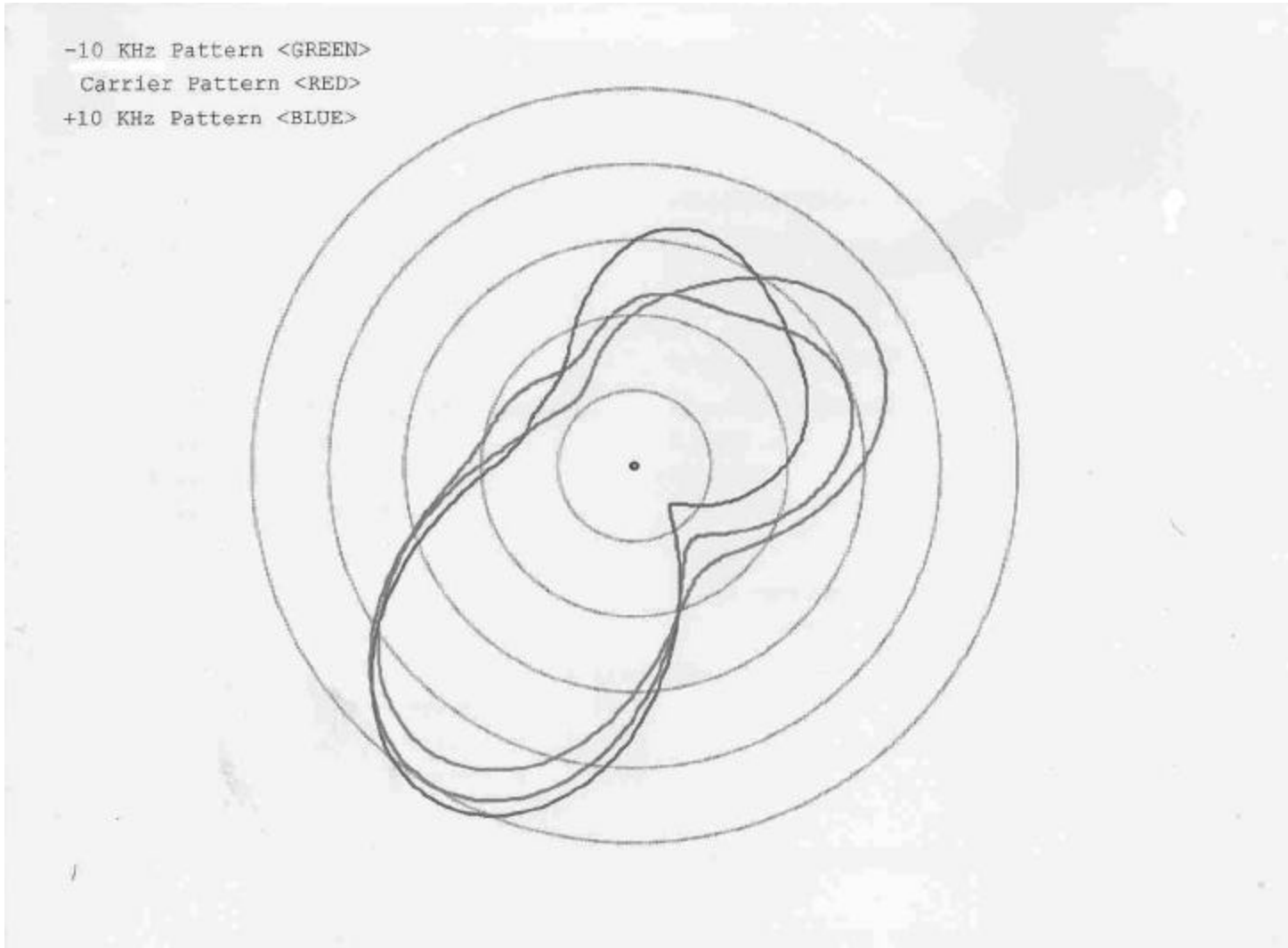


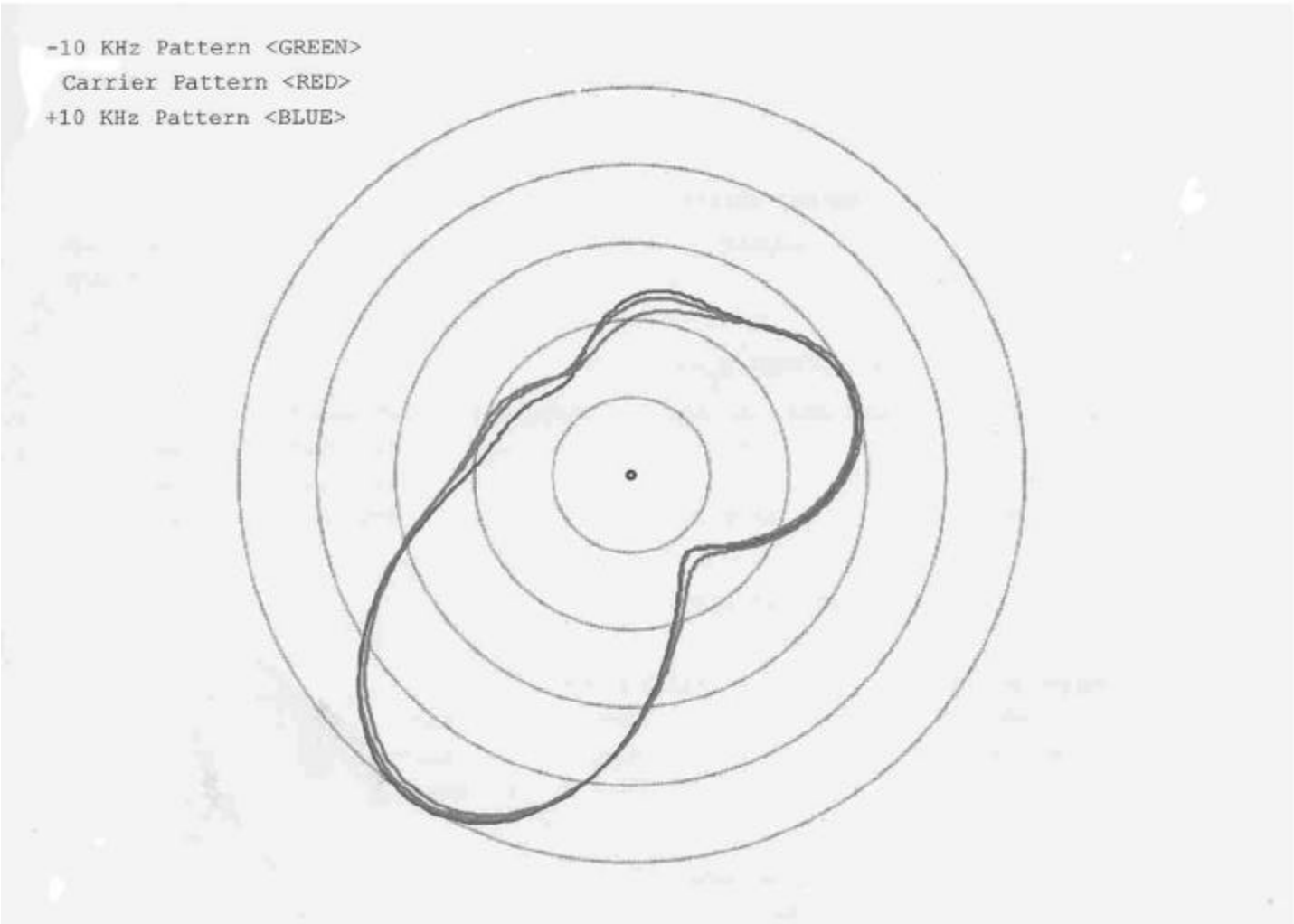
RMS = Pattern Size

$$**RSS = (E_1^2 + E_2^2 + \dots + E_n^2)^{1/2}**$$

**If E values are large
system is “sensitive” to small %
changes**

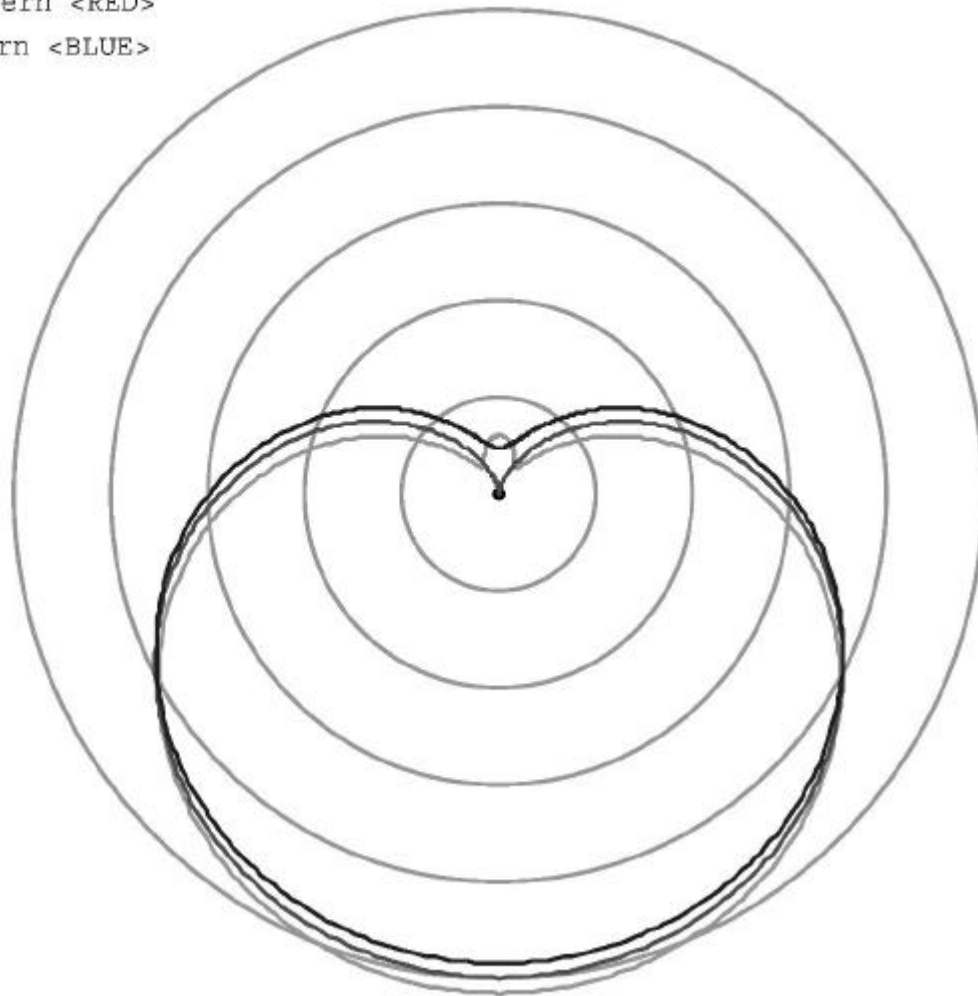
**If E values are small
system is more stable and has less
change with frequency (sidebands)**





INPUT IMPEDANCE RANGE FOR A SIMPLE PATTERN

-10 KHz Pattern <GREEN>
Carrier Pattern <RED>
+10 KHz Pattern <BLUE>



With simple straightforward feed system designs

	Lower VSWR	Upper VSWR
Example 1	1.11:1	2.17:1
Example 2	1.80:1	1.14:1
Example 3	2.17:1	1.18:1

The difference in feed system between Example 1 and Example 2 is only a 20 degree change in phase angle of the two ACU networks!

Best case for this simple feed system design

	Lower VSWR	Upper VSWR
Example 4	1.12:1	1.09:1
Input Z	45 +j2	48 -j4

Corrected with Phase Rotation Network to:

Input Z	46 +j3	47 -j3
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IBOC Review

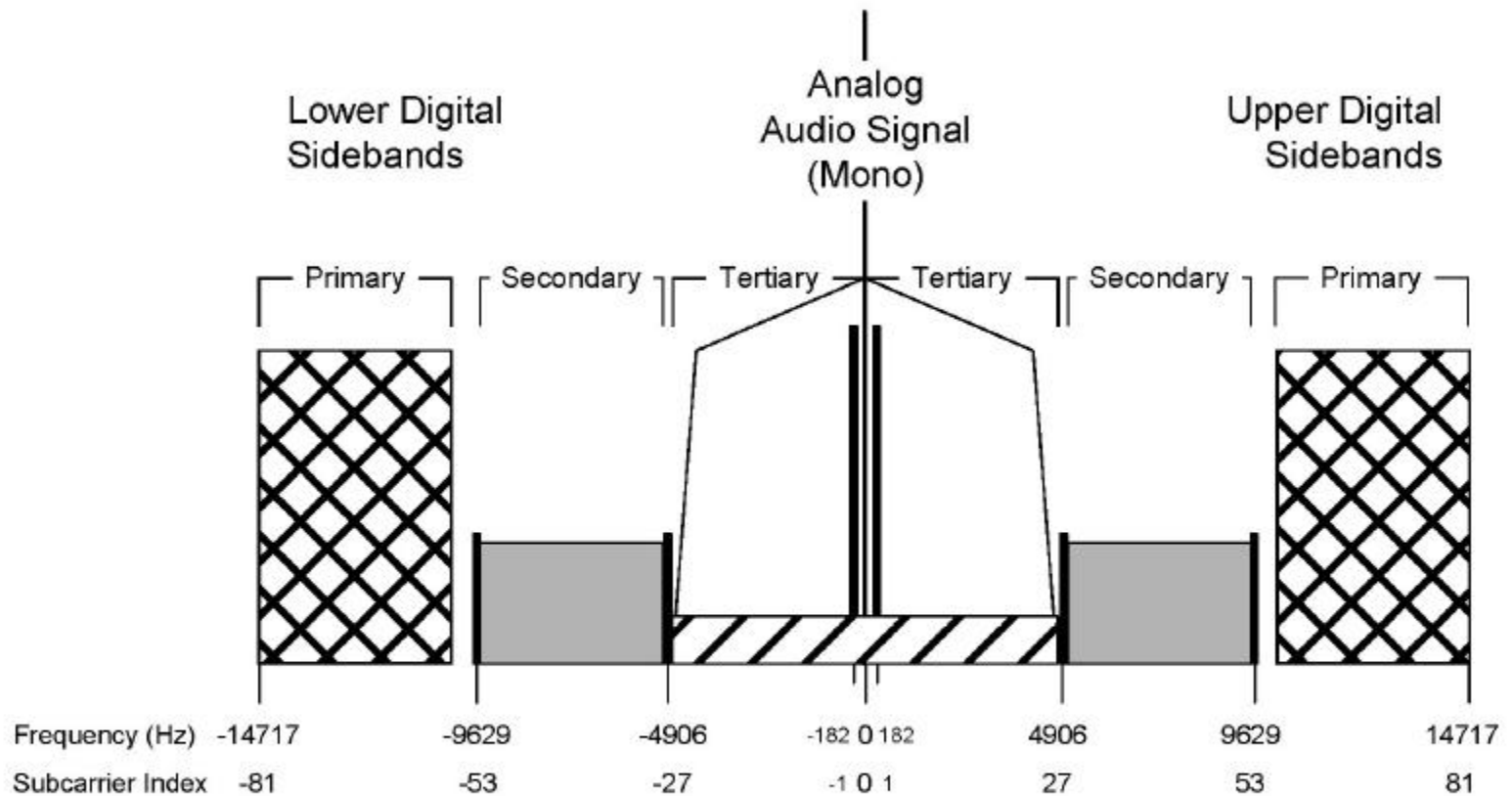


Figure 2 AM IBOC hybrid waveform spectrum.

Antenna Performance Concerns

- Unnecessarily High Digital-to-Analog Crosstalk (Hiss and “Bacon Frying” Sound)
- Decreased “Robustness” of Digital Signal
- Digital Coverage Area Limited by Pattern Bandwidth

Antenna Performance Concerns

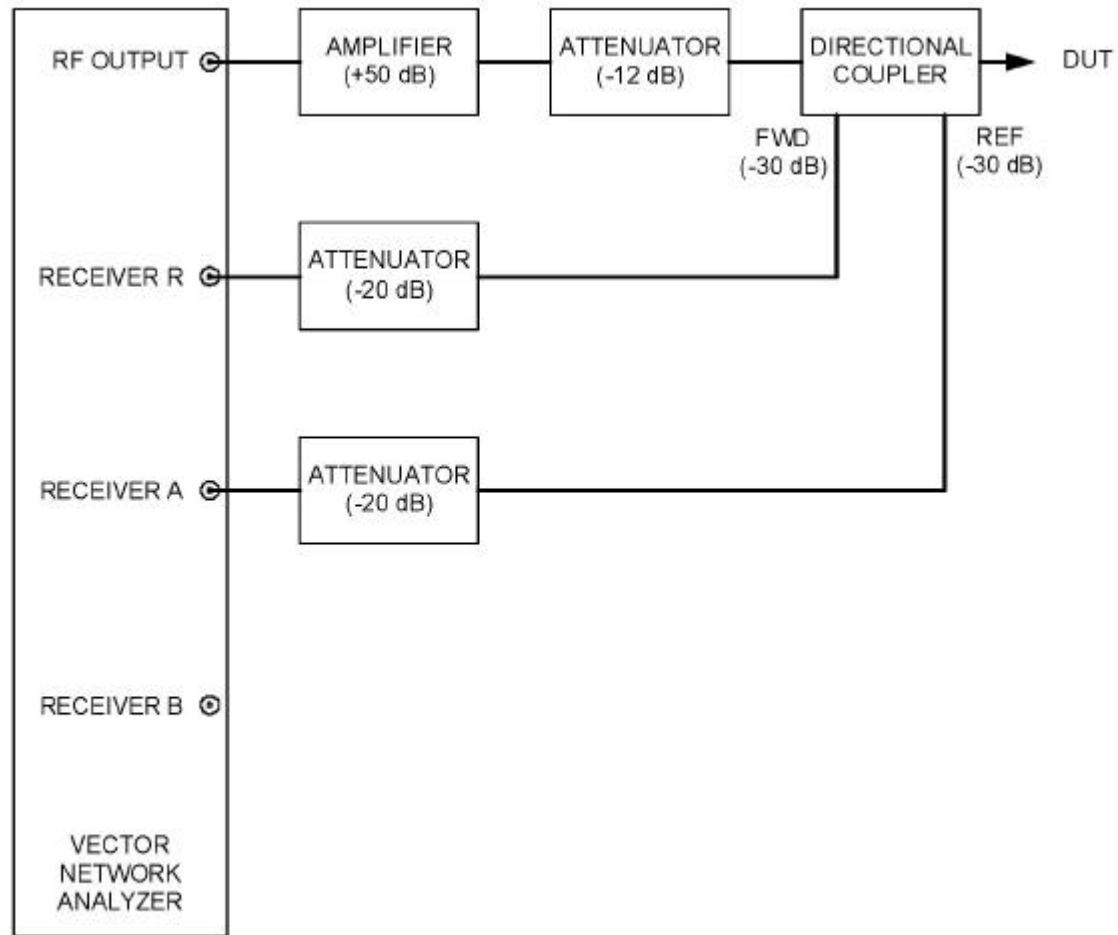
- Higher Adjacent Channel Interference Resulting from Poor Pattern Bandwidth
- Noisier Analog Reception in DA Null Region Due to Poor Pattern Bandwidth

IBOC Antenna System Requirements (as we know now)

- +/- 5 kHz – RF Final Amplifier Load Impedance Symmetry Such That VSWR of One Sideband Impedance Does Not Exceed 1.035:1 When Normalized to the Complex Conjugate of the Corresponding Sideband Impedance on the Other Side of Carrier Frequency (Hermitian Symmetry)

IBOC Antenna System Requirements (as we know now)

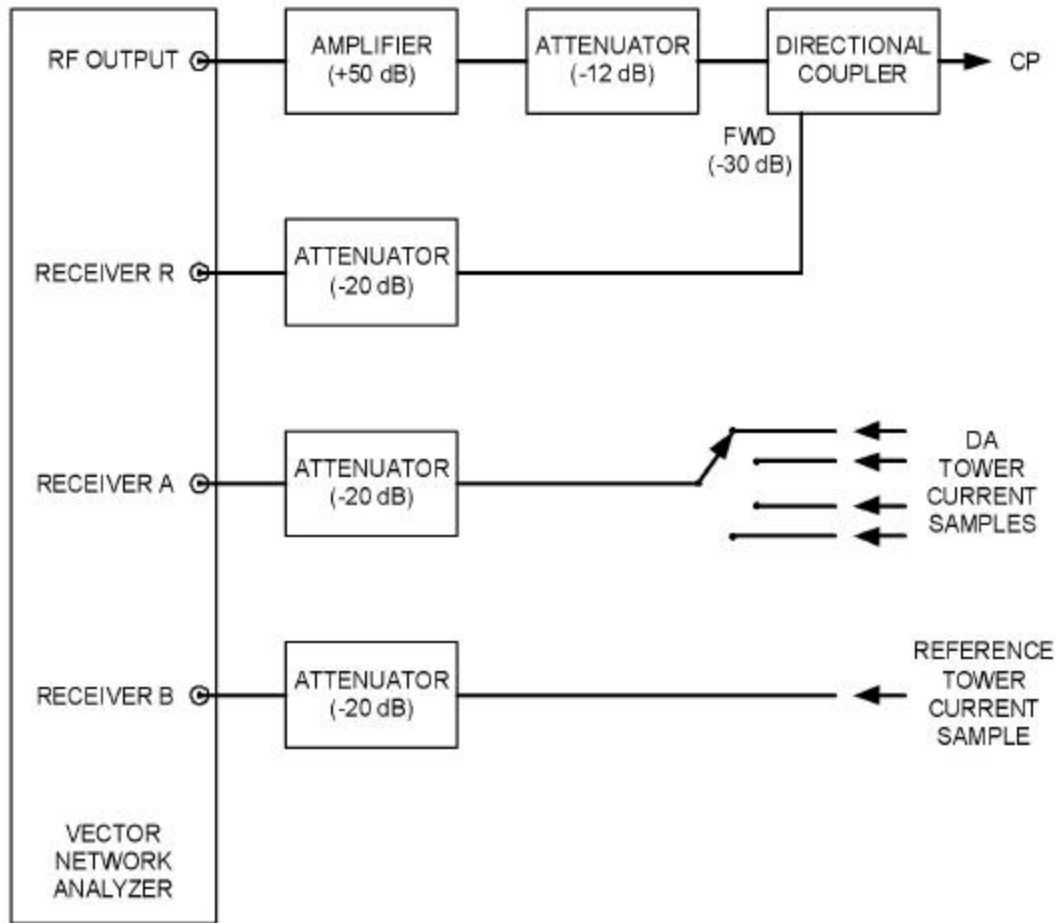
- +/- 10 kHz – RF Final Amplifier Load
Impedance VSWR Not Exceeding 1.20:1
- +/- 15 kHz – RF Final Amplifier Load
Impedance VSWR Not Exceeding 1.40:1



Input Impedance Measurement System

IBOC Antenna System Requirements (as we know now) Cont.

- For Directional Antennas
 - Amplitude Response of +/- 2 dB across the 30 kHz Bandwidth
 - Phase Response of less than 27° across the 30 kHz of Bandwidth



Antenna Array Parameter Measurement System

Directional Antenna Analysis

- System Measurements +/- 30 kHz
Measured on Sample System
- Measurements used in MiniNEC model to
determine Far-Field Performance

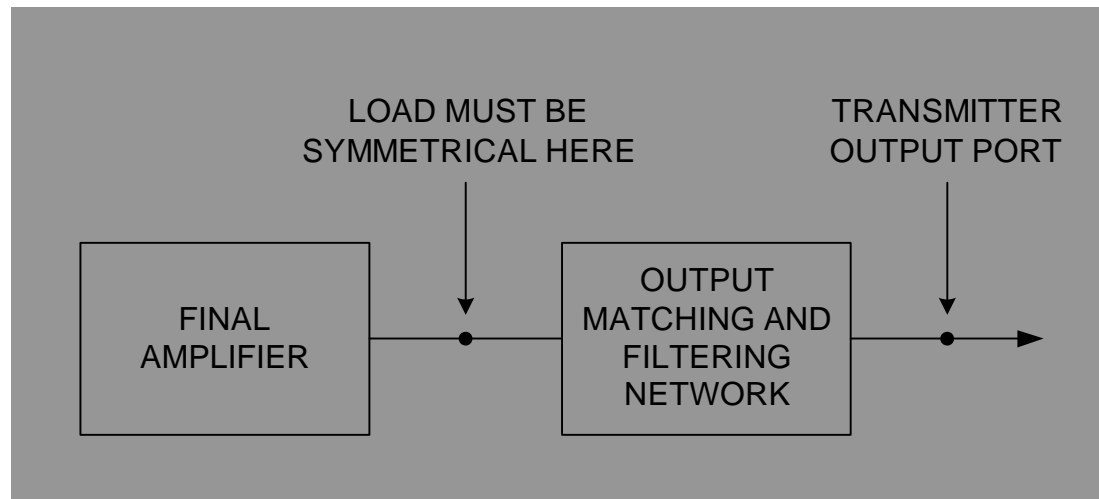
DRM Antenna System Requirements

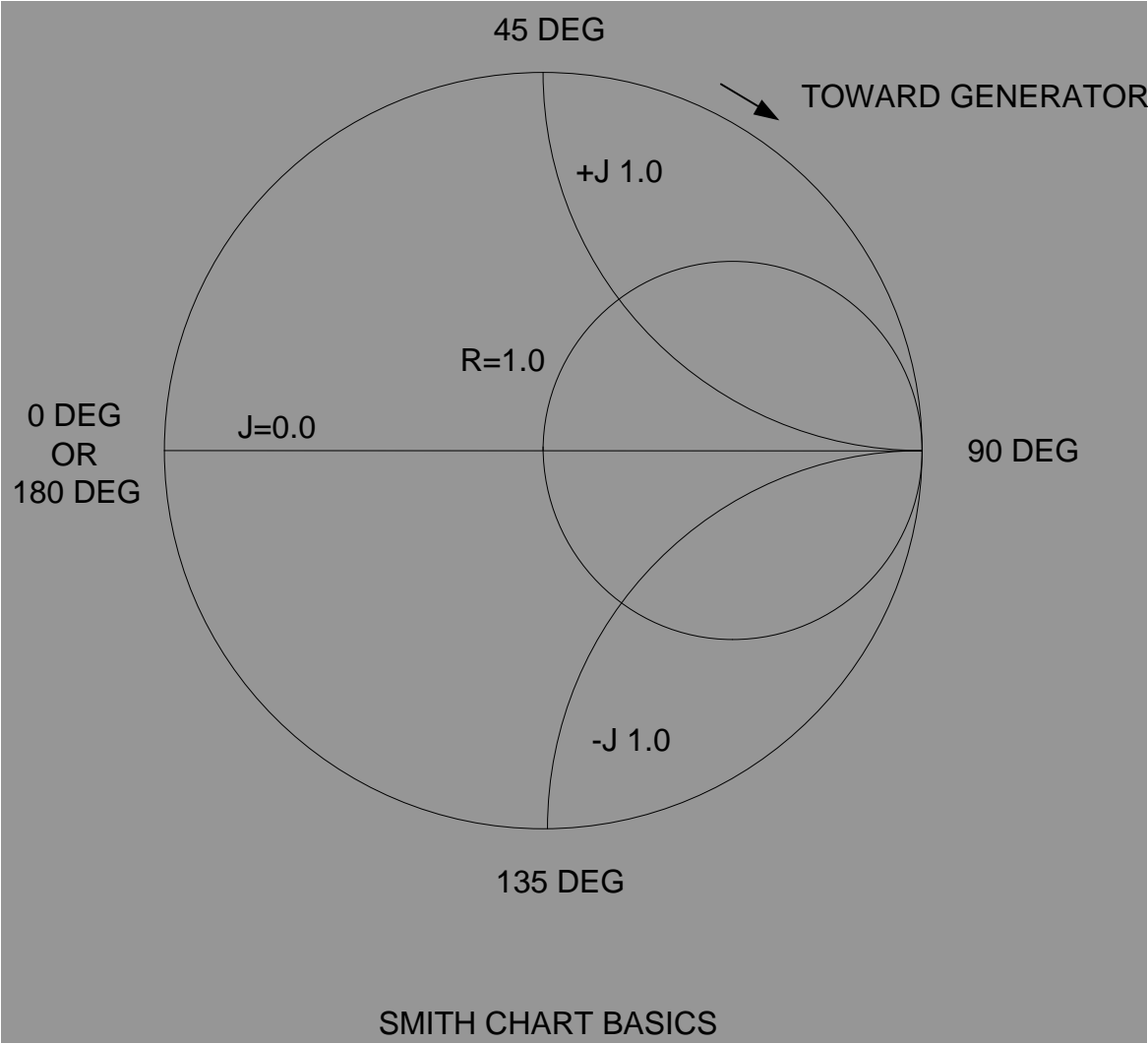
- +/- 10 kHz –VSWR Not Exceeding 1.20:1
- +/- 15 kHz –VSWR Not Exceeding 1.40:1
- Hermitian Symmetry
- Re-injection of suppressed carrier may also be used in cases where bandwidth is limited

Optimizing Load Impedance

- Reduces Noise from Digital-To-Analog Crosstalk
- Improves Spectral Purity of Digital Signal
- Improves Headroom for Receiver Error Correction

Final Amplifier Load Optimization



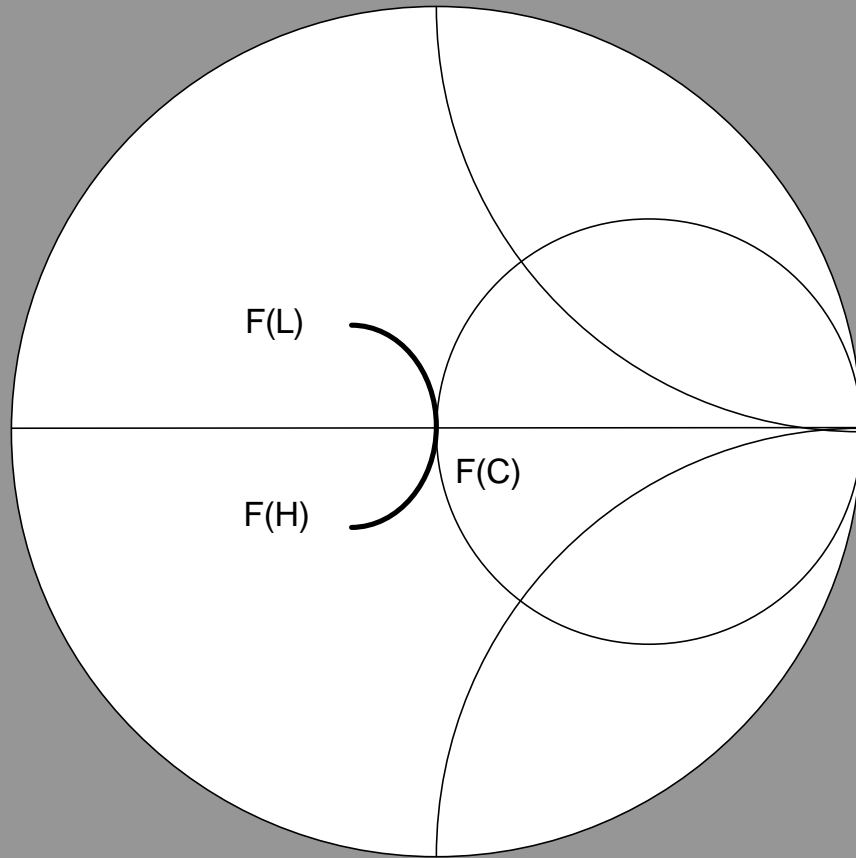


Normalizing Per-Unit Values of Impedance

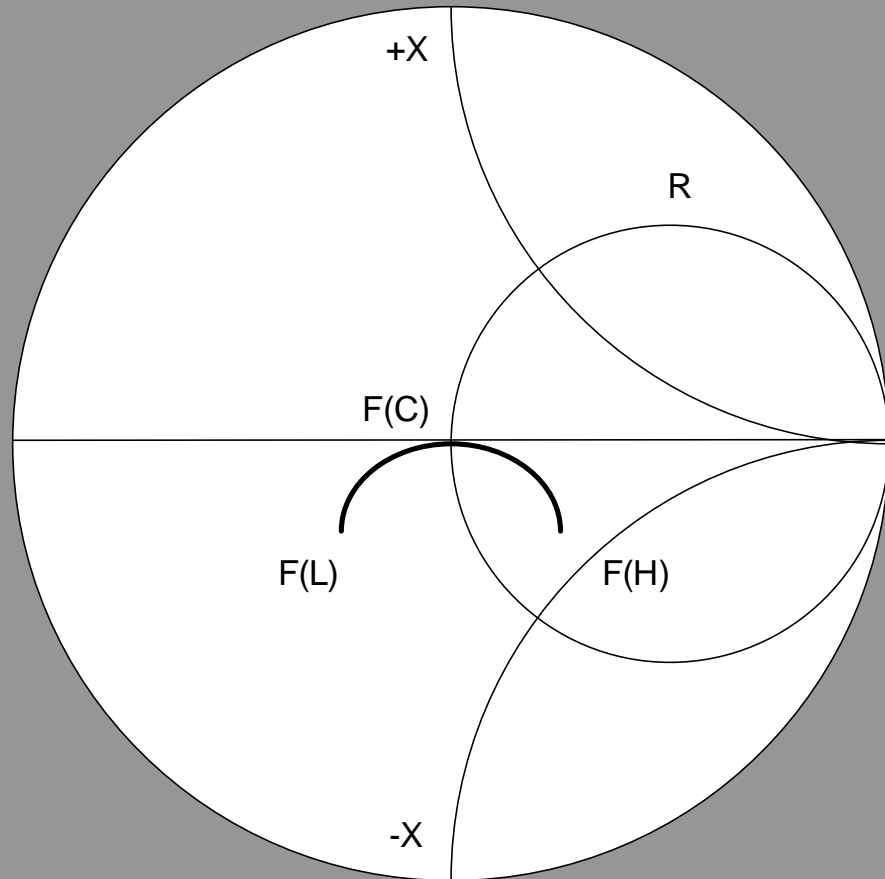
- Divide Each Sideband Resistance by the Carrier Resistance
- Divide the Difference Between Each Sideband Reactance and the Carrier Reactance by the Carrier Resistance

Normalizing Examples

Frequency	Resistance	Reactance	Per-Unit Resistance	Per-Unit Reactance
-15 kHz	45.0	-j 8.0	0.90	-j 0.16
Carrier	50.0	j 0.0	1.00	j 0.00
+15 kHz	57.0	+j 10.0	1.14	+j 0.20
-15 kHz	45.0	-j 8.0	0.86	-j 0.09
Carrier	52.5	-j 3.5	1.00	j 0.00
+15 kHz	57.0	+j 10.0	1.09	+j 0.12

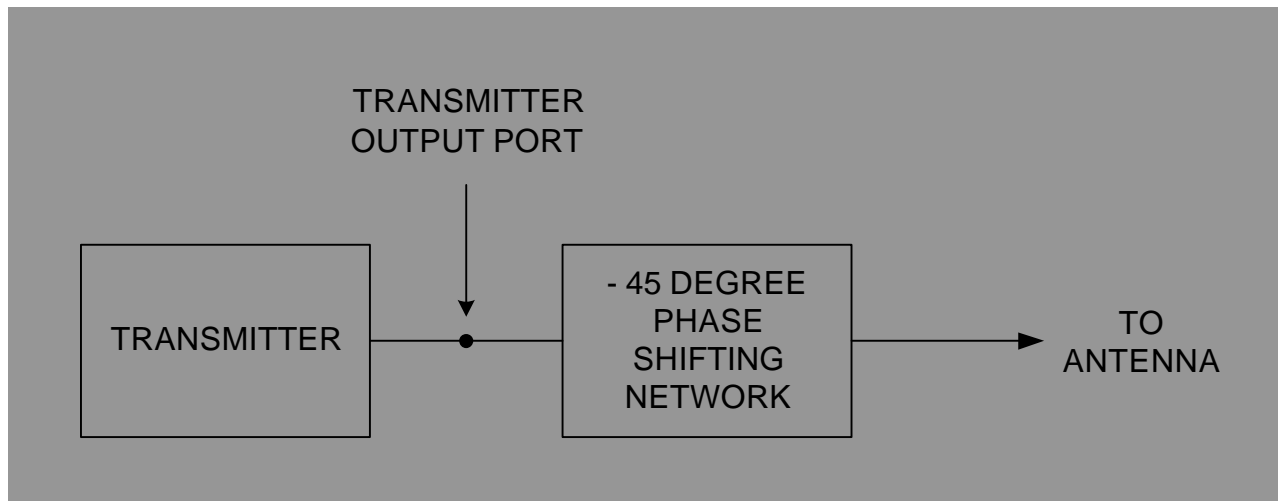


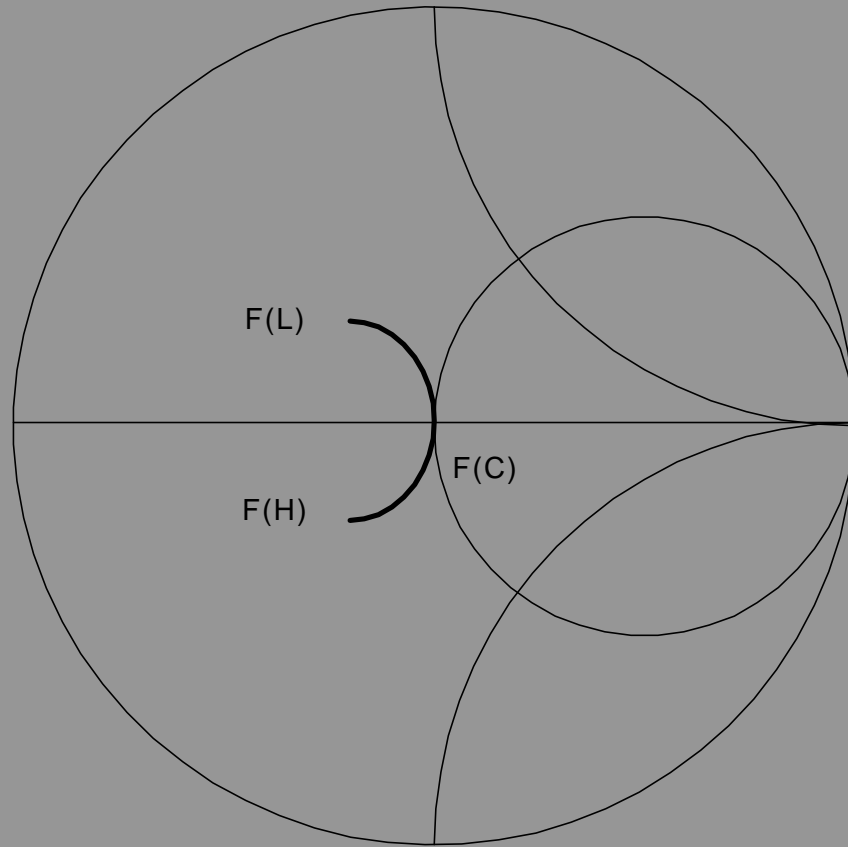
FINAL AMPLIFIER LOAD IMPEDANCE SYMMETRY



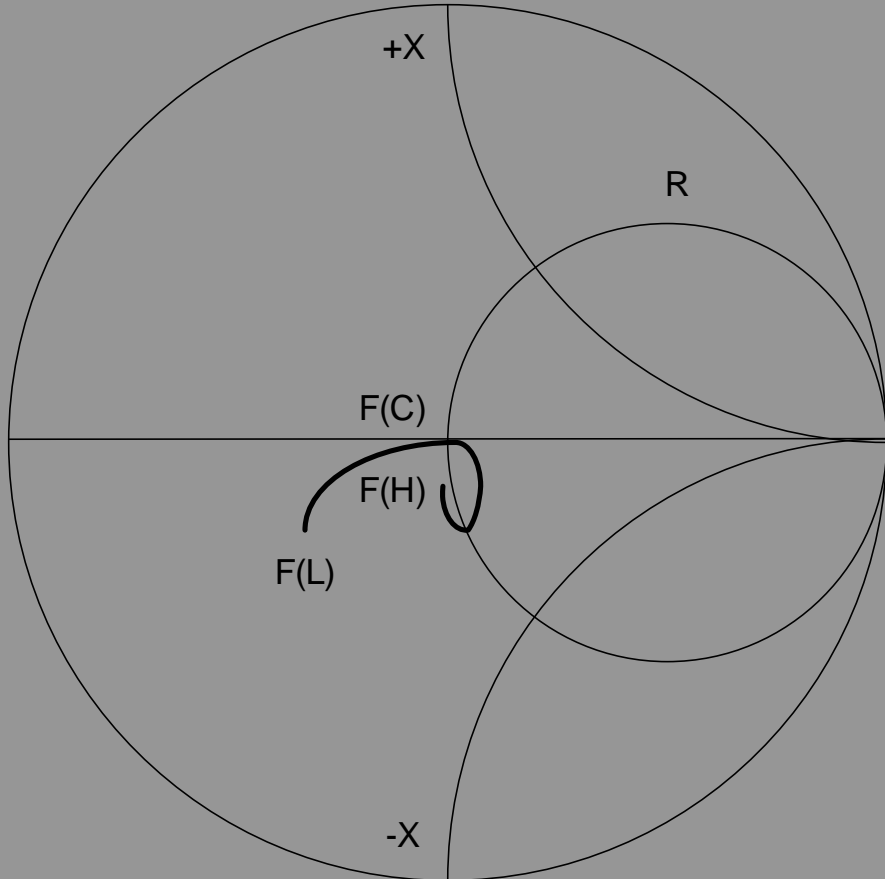
FINAL AMPLIFIER
LOAD IMPEDANCE ASSYMMETRY

Phase Rotation Network



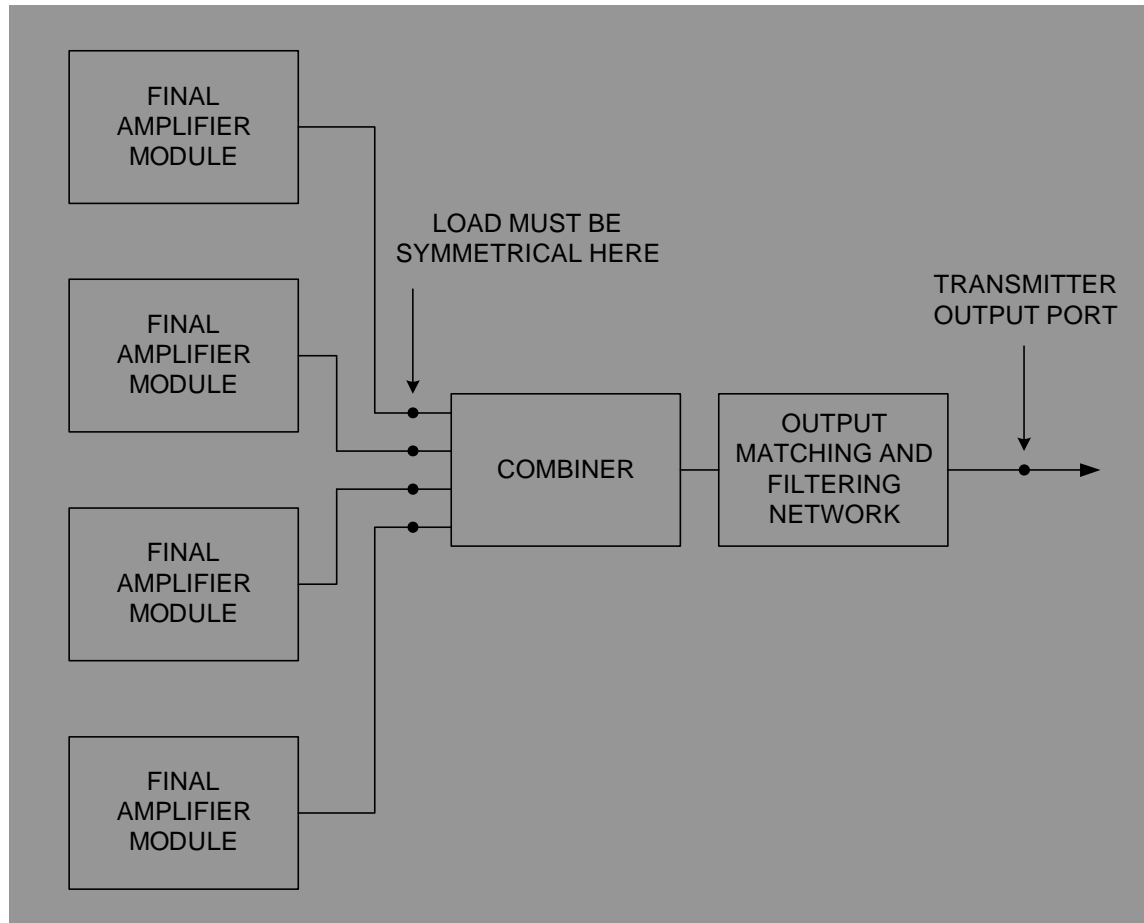


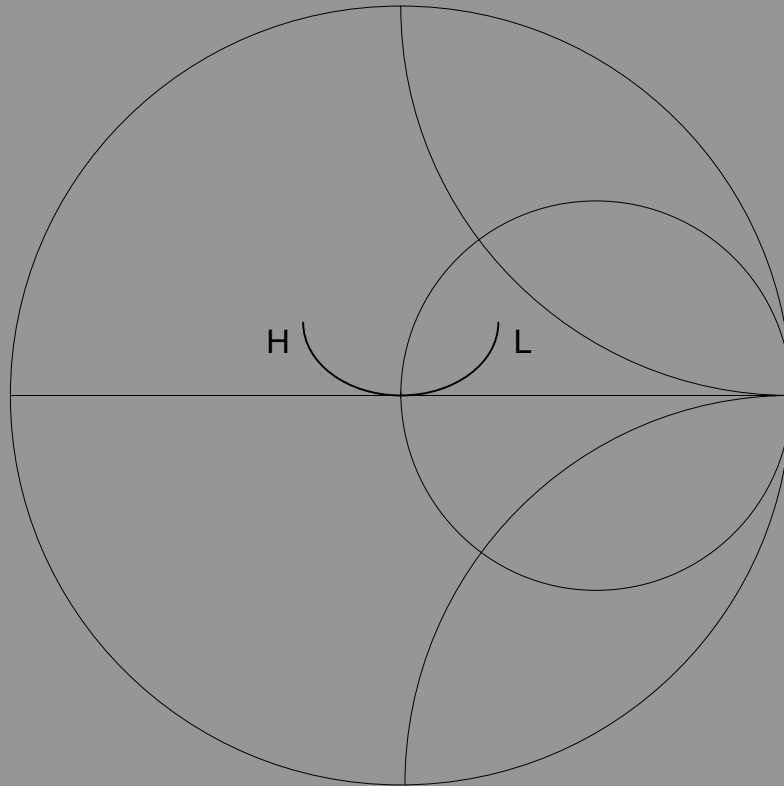
FINAL AMPLIFIER LOAD IMPEDANCE SYMMETRY



UNCORRECTABLE IMPEDANCE ASYMMETRY

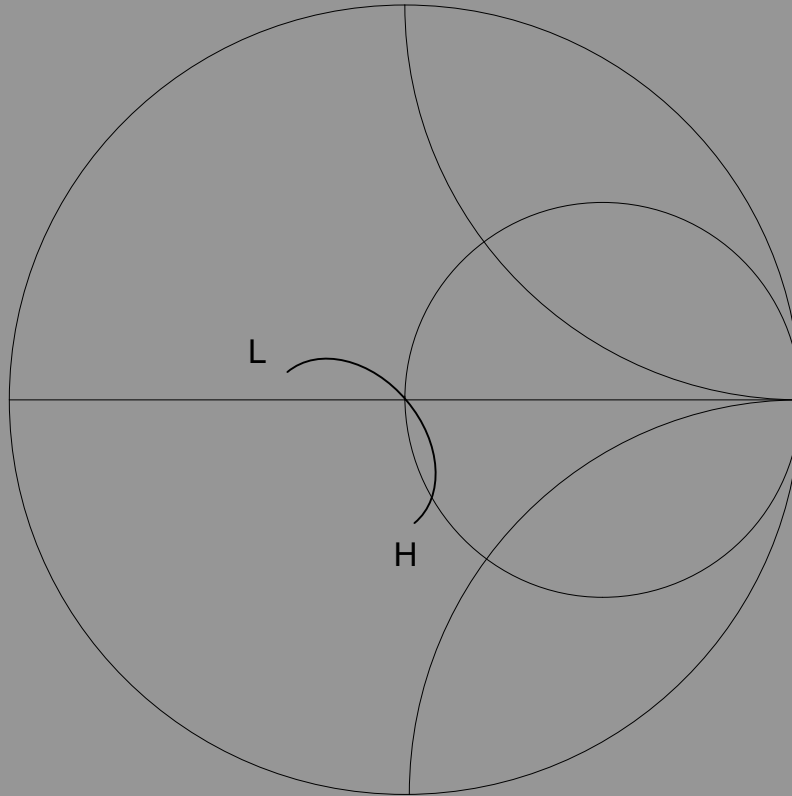
Transmitters With Transformer Combiners





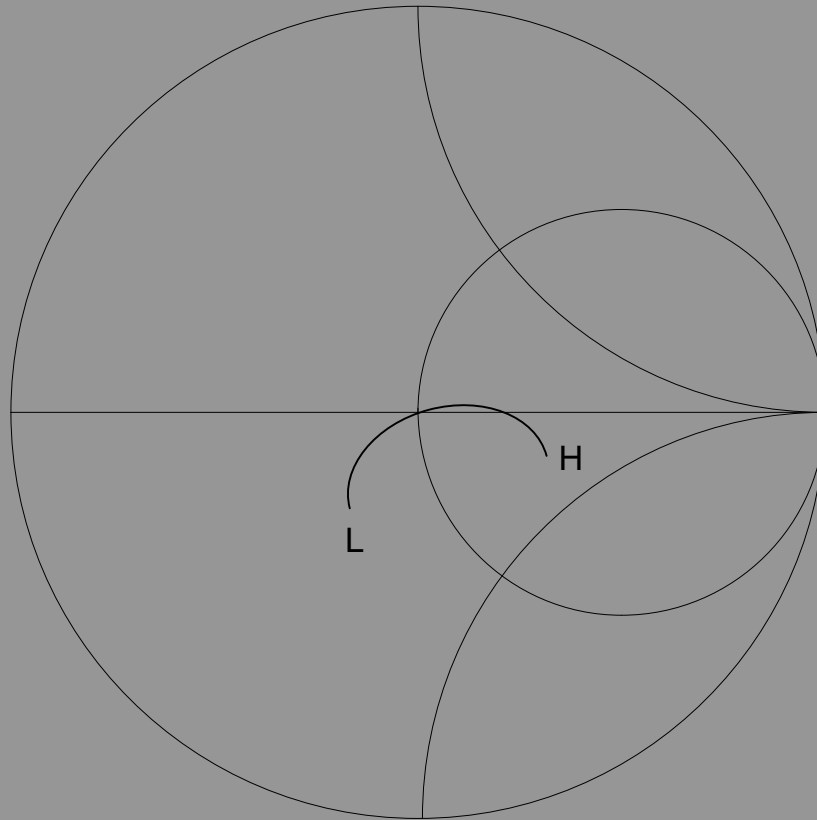
SYMMETRICAL SIDEBAND LOAD
FOR TRANSMITTER WITH
-135 DEGREE OUTPUT NETWORK

(MOST HARRIS MODELS)



SYMMETRICAL SIDEBAND LOAD
FOR TRANSMITTER WITH
-200 DEGREE OUTPUT NETWORK

(MOST BE MODELS)

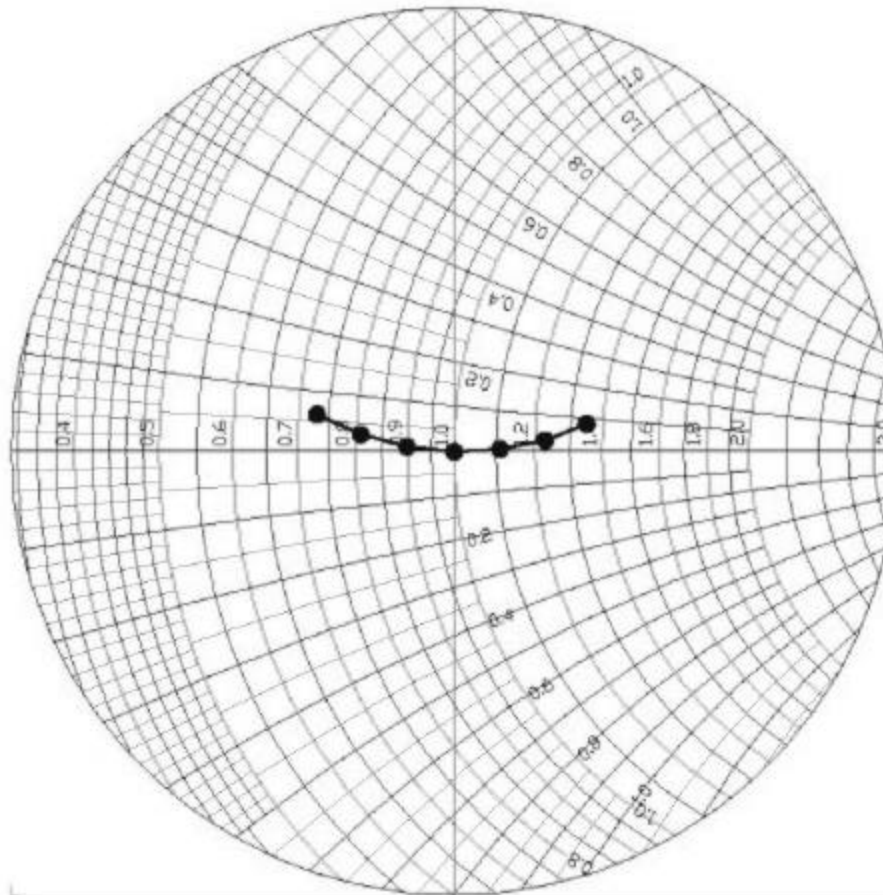


SYMMETRICAL SIDEBAND LOAD
FOR TRANSMITTER WITH
-60 DEGREE OUTPUT NETWORK

(NAUTEL MODELS?)

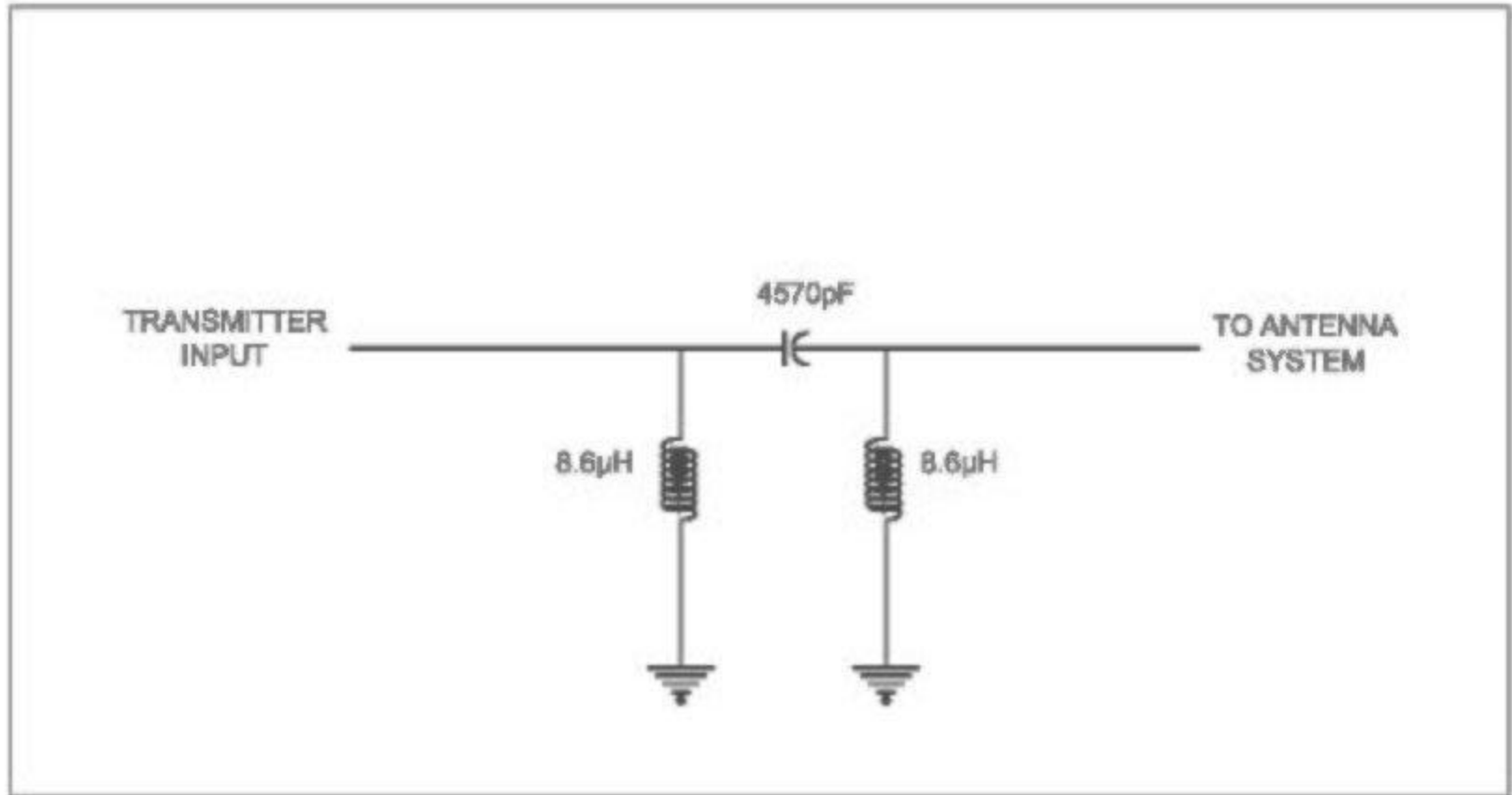
KOTZ

Frequency (kHz)	Impedance		VSWR	IBOC	
	Resistance	Reactance		VSWR	Symmetry
705	67.5	4.4	1.363	Yes	
710	61.4	1.6	1.231	No	
715	55.5	0.4	1.110	Yes	
720	50.0	0.0	1.000		No
725	45.0	0.6	1.112	Yes	
730	40.4	1.7	1.241	No	
735	36.5	3.2	1.381	Yes	

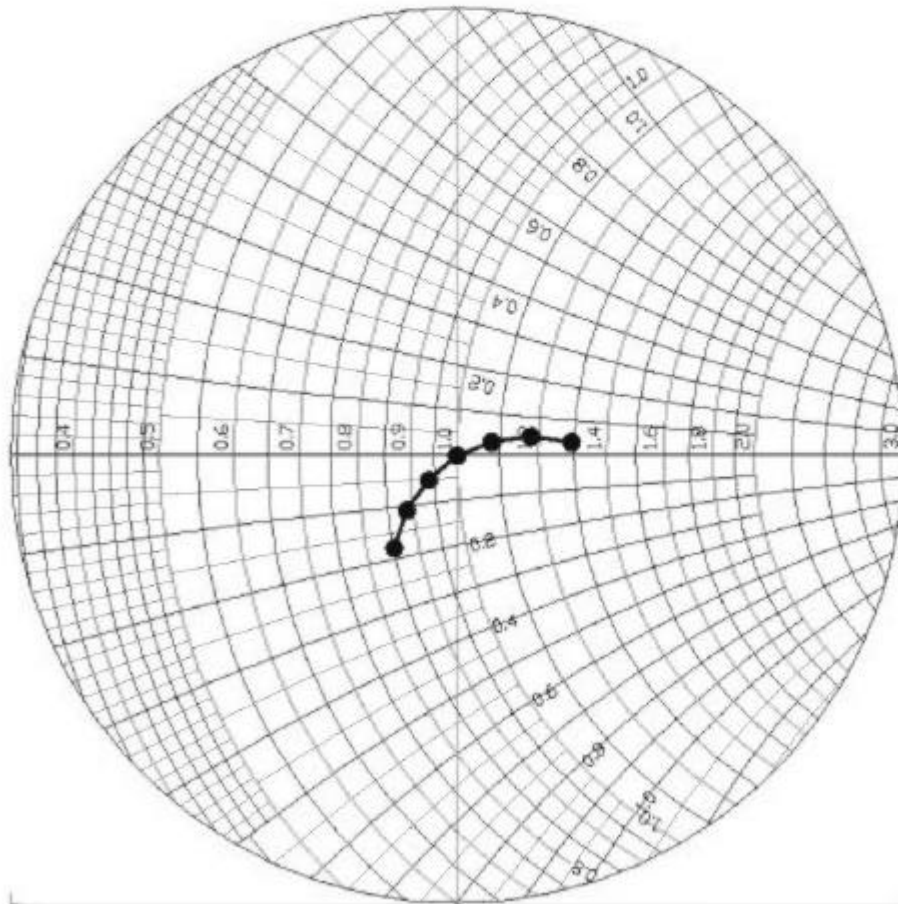


Load At Antenna Feed Line

104.5° Rotation

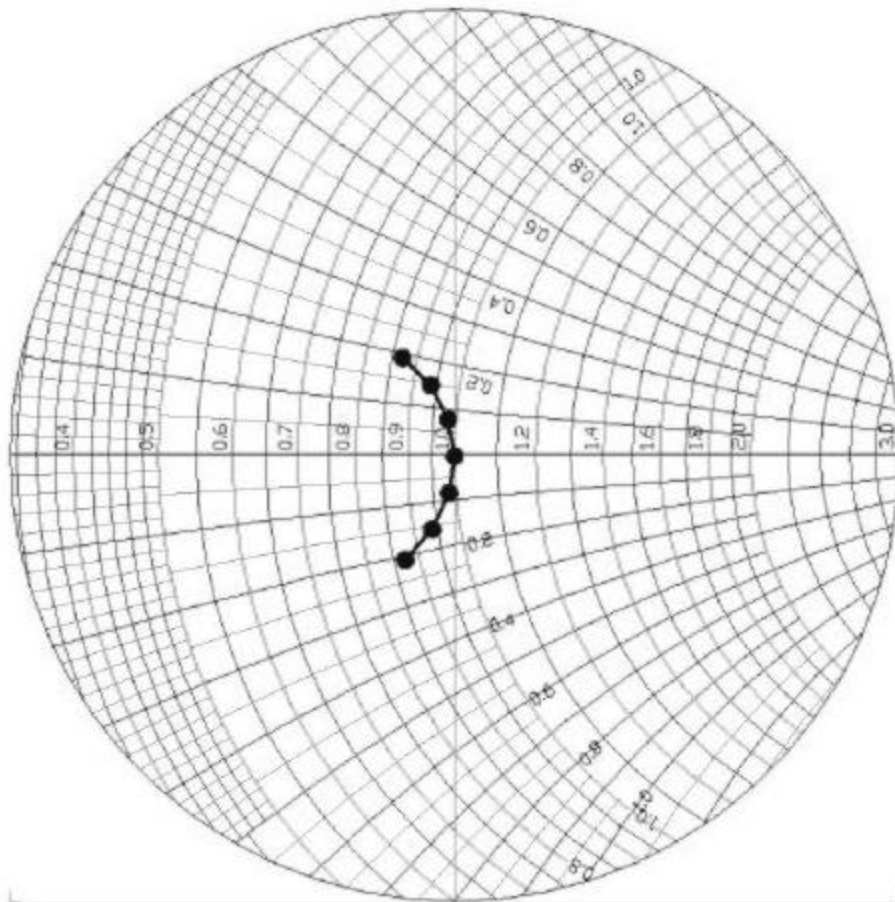


Frequency (kHz)	Impedance Resistance	Reactance	VSWR	IBOC VSWR	IBOC Symmetry	VSWR
705	42.6	-8.9	1.285	Yes		
710	44.3	-5.4	1.181	Yes		
715	46.8	-2.5	1.087	Yes		
720	50.0	0.0	1.000		No	1.155
725	54.0	1.7	1.088	Yes		
730	59.0	2.6	1.188	Yes		
735	64.6	2.0	1.296	Yes		

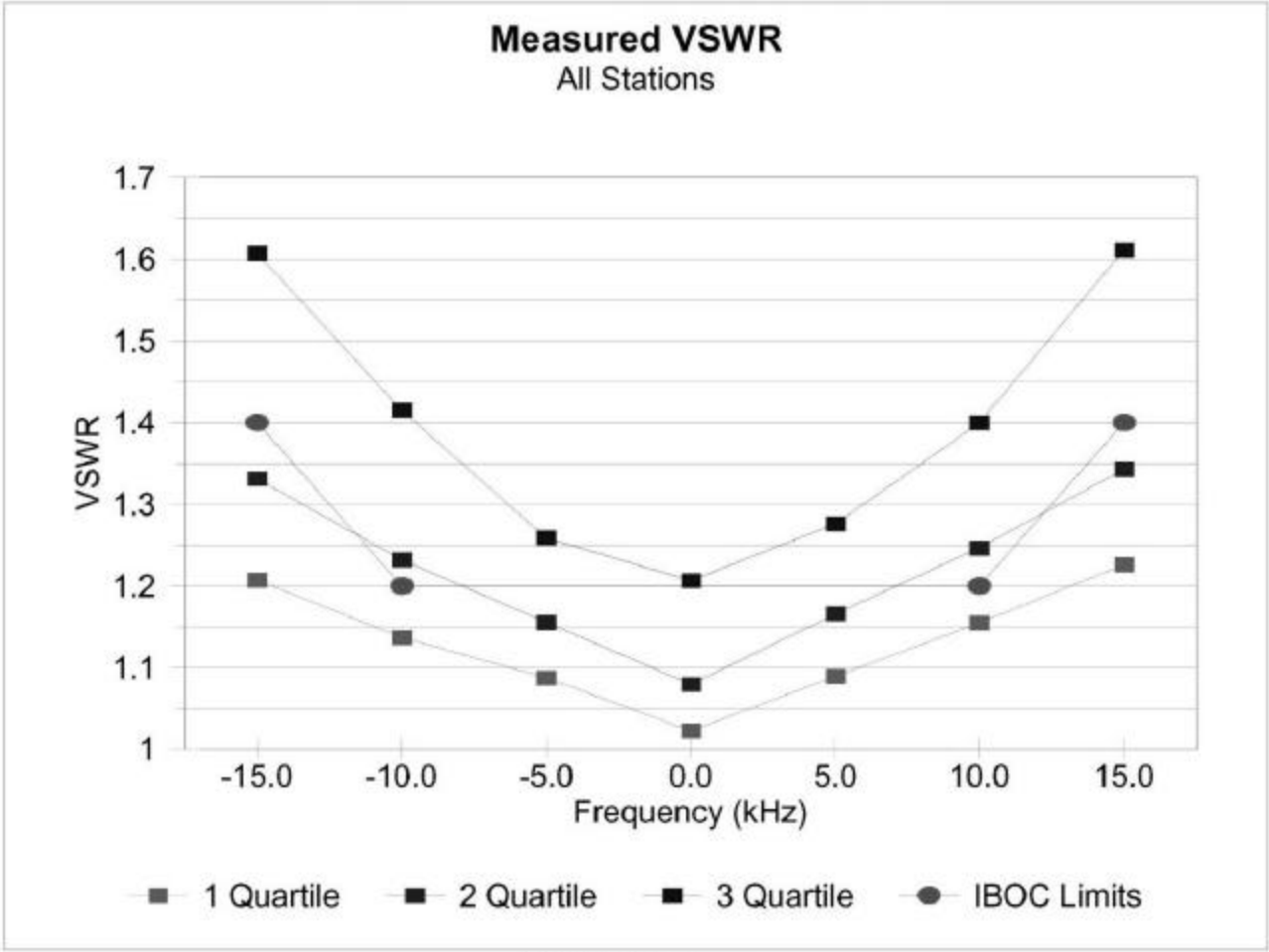


Load Rotated Through Phase Rotation Network

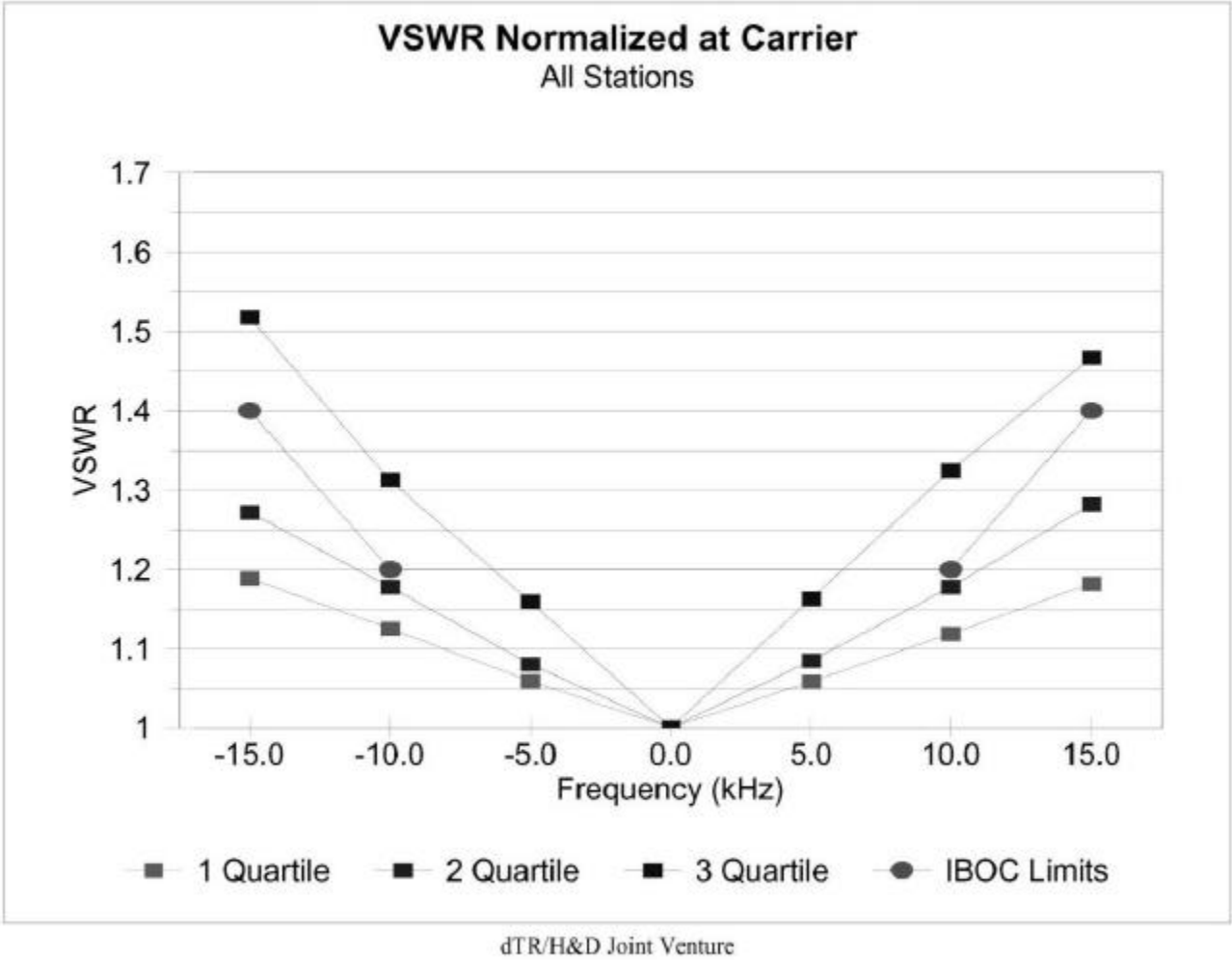
Frequency (kHz)	Impedance Resistance	Impedance Reactance	VSWR	IBOC VSWR	IBOC Symmetry	IBOC VSWR
705	43.5	9.7	1.285	Yes		
710	46.8	7.4	1.181	Yes		
715	49.1	4.0	1.087	Yes		
720	50.0	-0.0	1.000		Yes	1.003
725	49.2	-4.1	1.088	Yes		
730	46.9	-7.8	1.188	Yes		
735	43.6	-10.3	1.296	Yes		

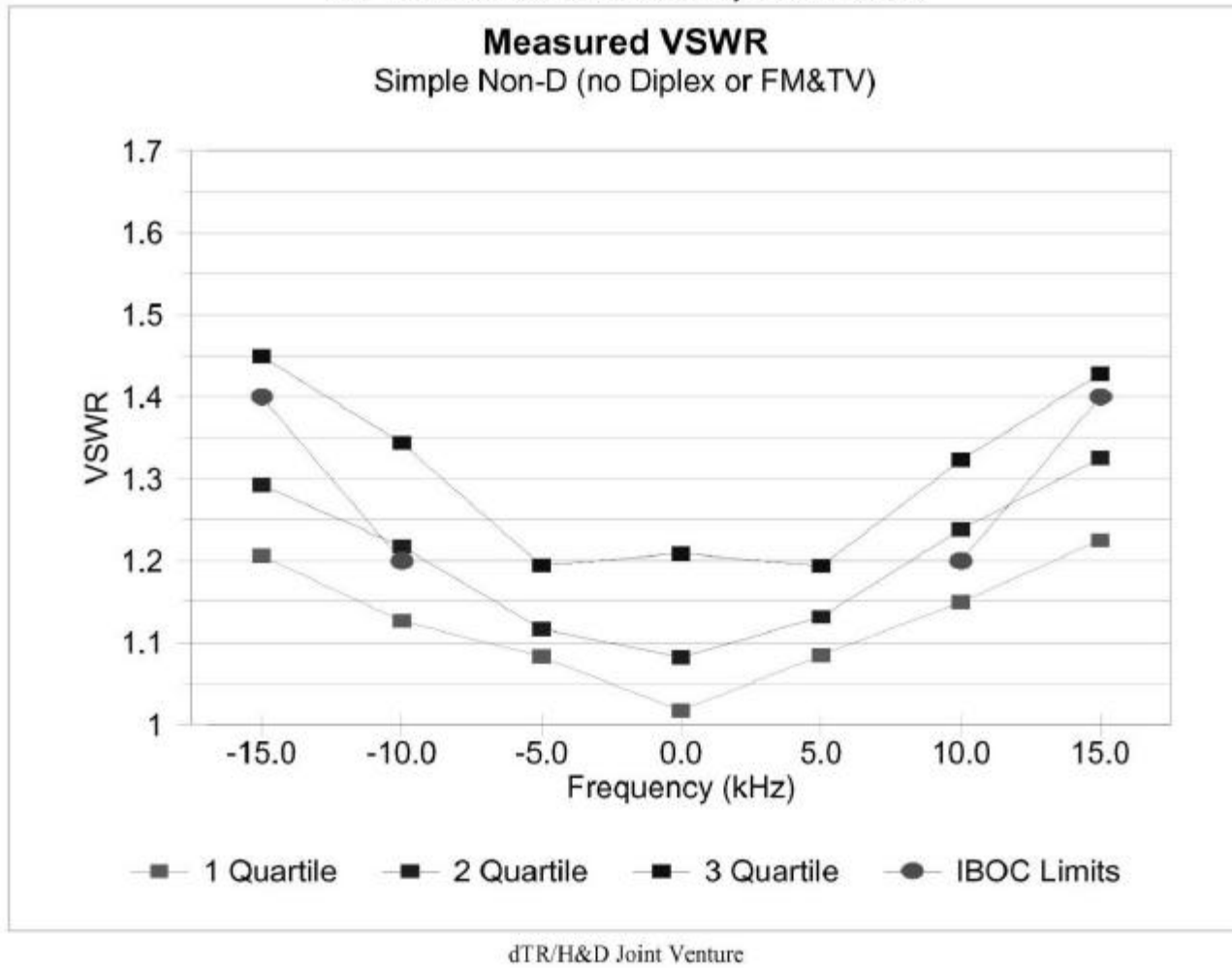


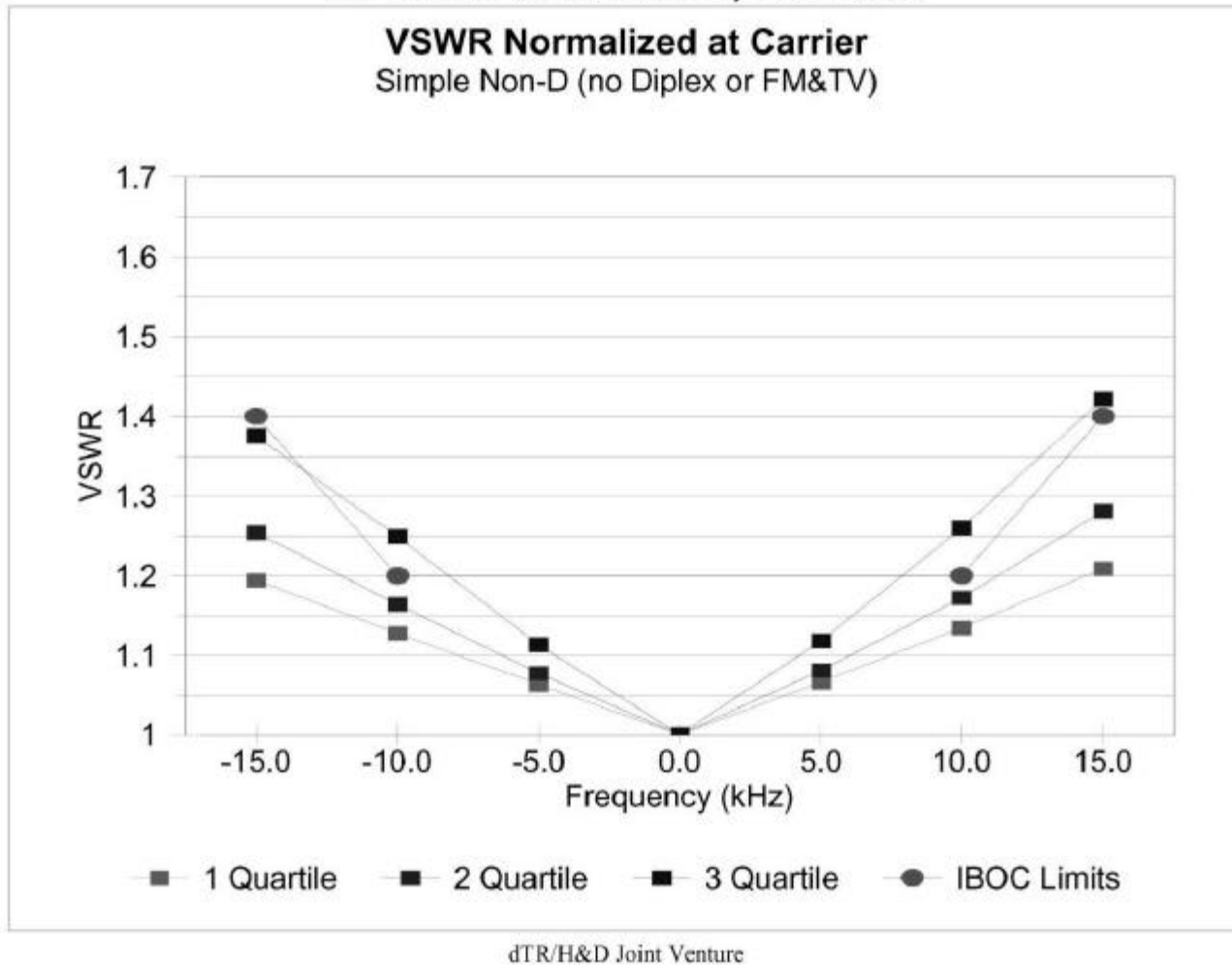
Load Rotated in Transmitter Output Network

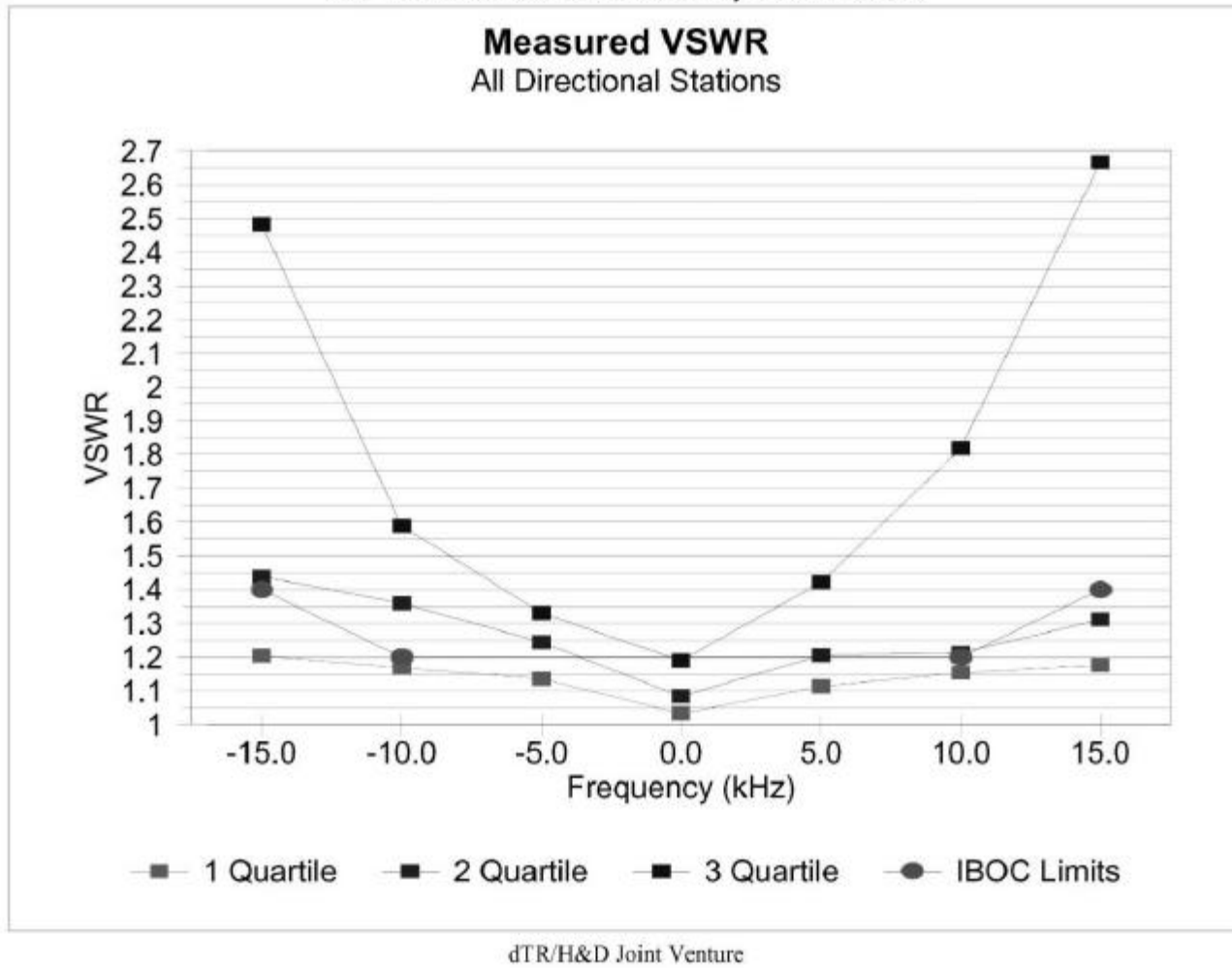


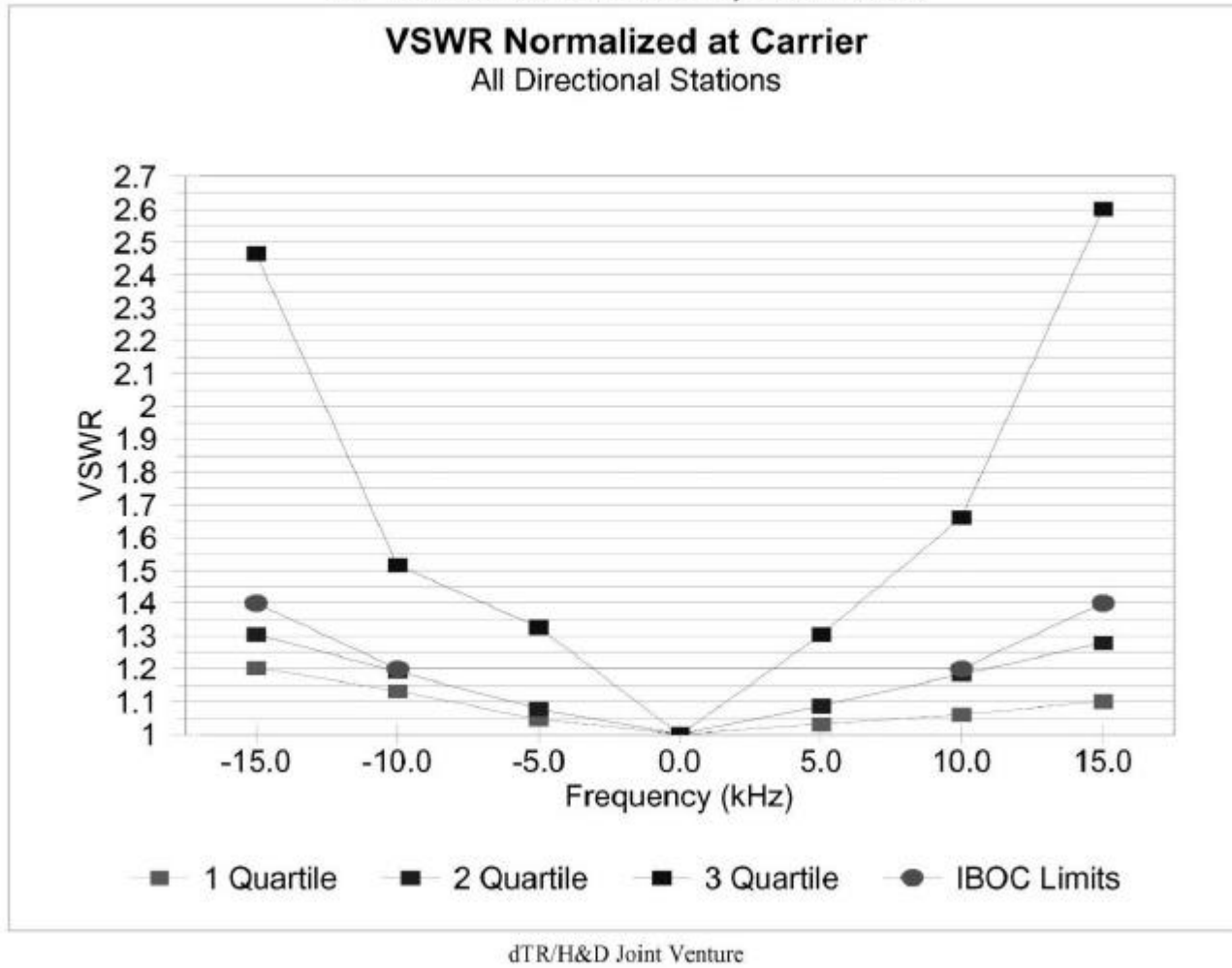
dTR/H&D Joint Venture

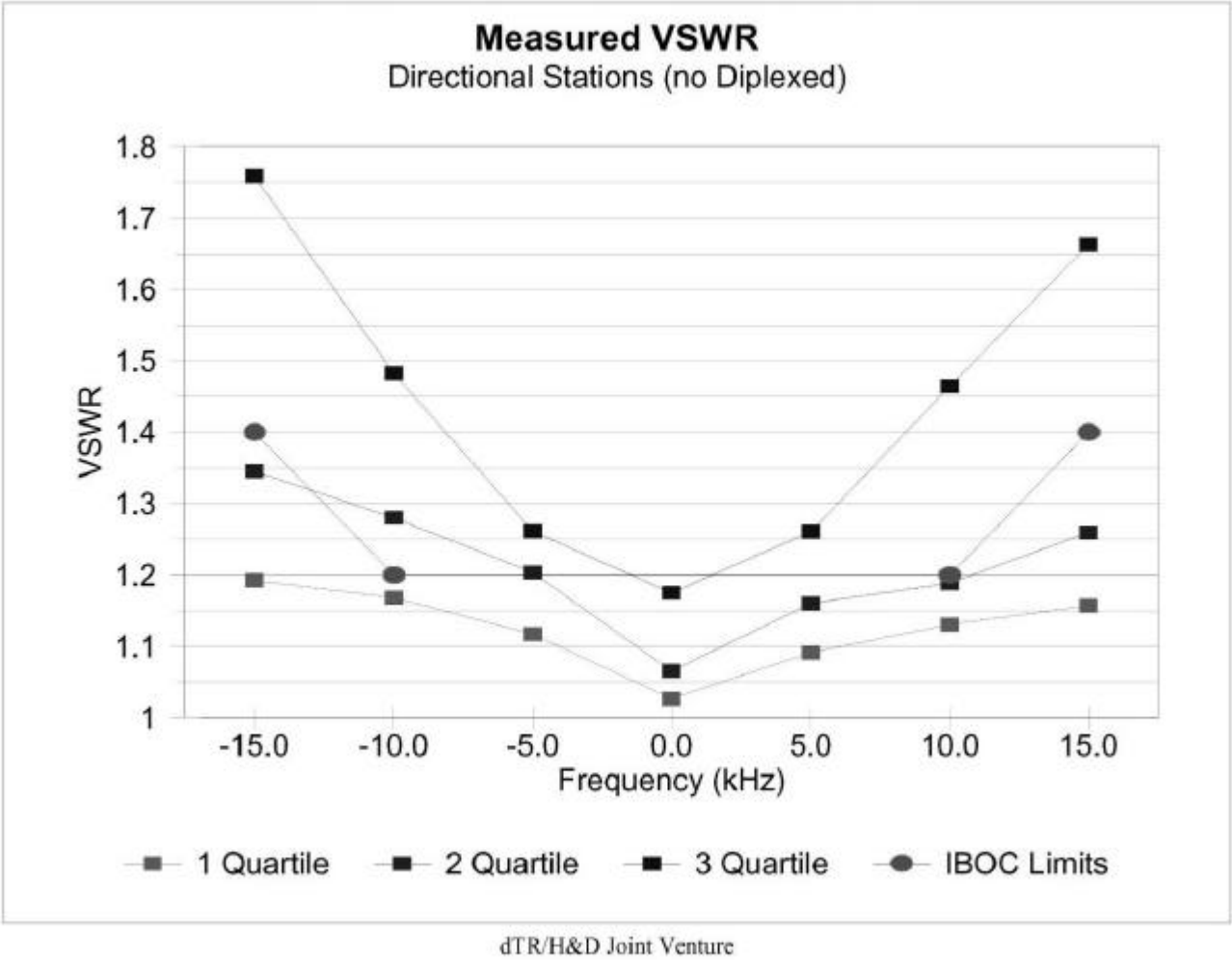


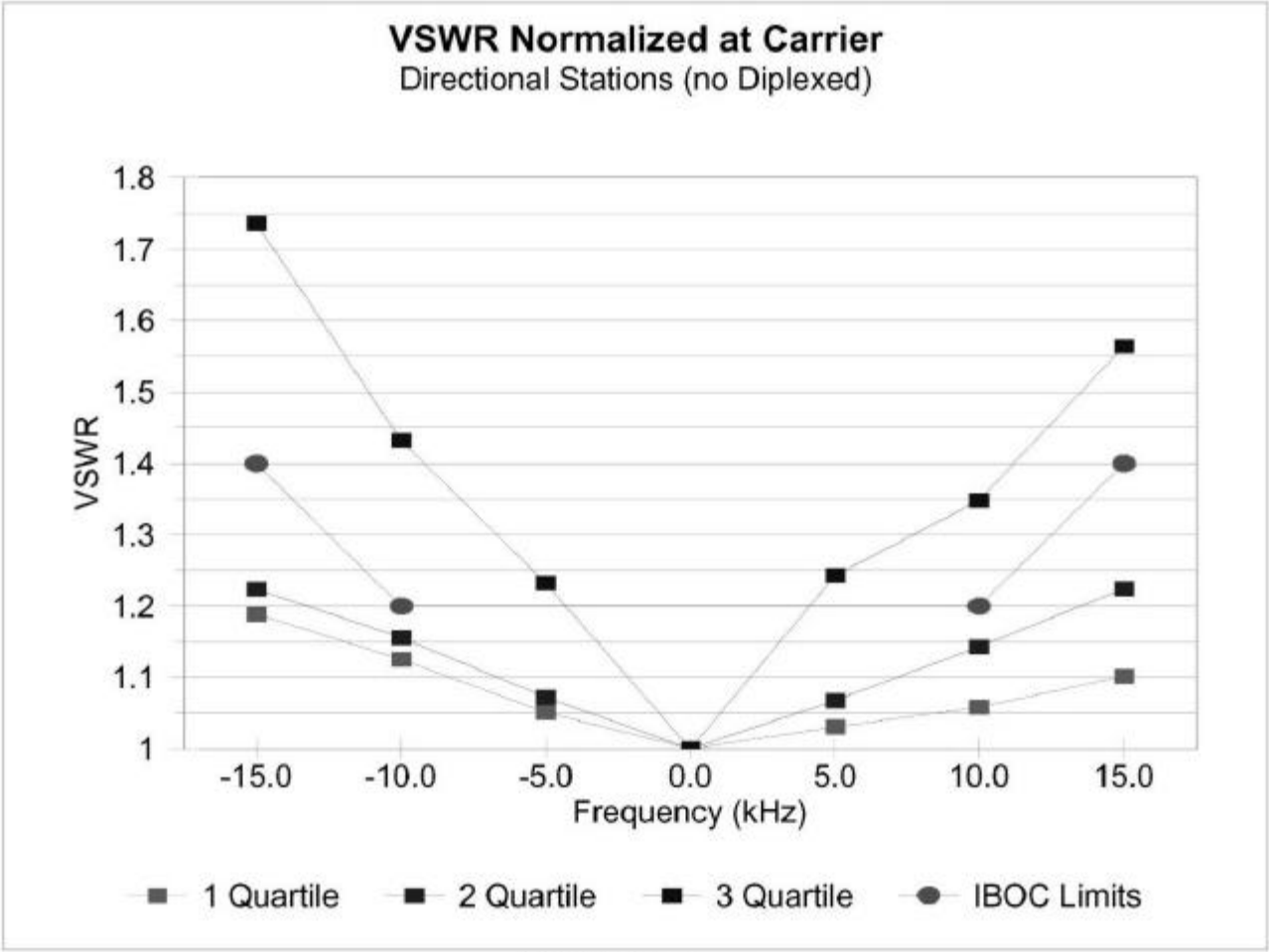




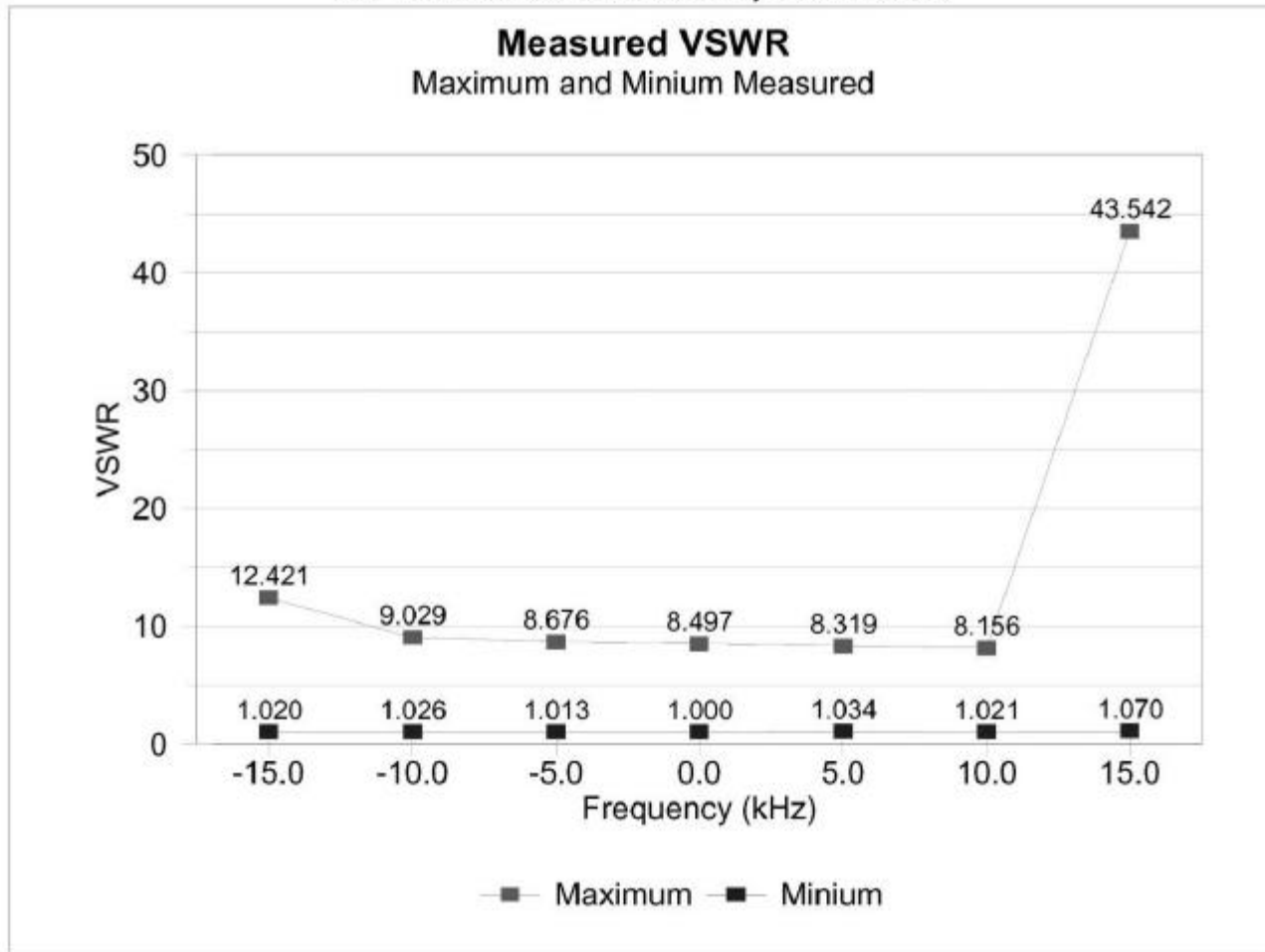








dTR/H&D Joint Venture



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Important Findings

- Poor Maintenance (or complete lack of any maintenance)
- Low power due to wrong operating impedance
- Bad modulation due to wrong operating impedance
- Patterns out of adjustment

Maintenance

- IBOC readiness allows attention to other critical infrastructure issues
- Do you buy a new transmitter to put it in a garden shed with a leaky roof?
- Is it time to improve?
 - Electrical service
 - Fencing
 - Security
 - Grounding
 - Etc.

Where to Go From Here

- Transmitter Manufactures are Thinking About This Problem – Adaptive Equalization
- Not Pass-Fail Test – IBOC Signal Has Redundancy
- See What Happens

Where to Go From Here

- Use the Report to design optimal feed system for the selected IBOC transmitter
- Alaska (Public Stations along with Alaska Broadcasters Association) Could Propose a State Wide STA or Waiver to Use IBOC For Daytime and Nighttime to Test Nighttime Operation

Questions?

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